

Description

Method for cooling a turbo machine and turbo machine for it

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The invention relates to a method for cooling thermally stressed regions in a turbo machine which has a live-steam feed line, an inflow region, a housing and an exhaust-steam region, a flow medium flowing through the 10 turbo machine and leaving in the exhaust-steam region during operation, and also relates to a turbo machine for carrying out the method.

In the construction of turbo machines, especially in 15 the construction of steam turbines, steam at temperatures lying below the temperature of live steam under live steam pressure is required for cooling regions that are subjected to high thermal stress. The live steam pressure is the pressure of a flow medium 20 entering the inflow region of a turbo machine. The live steam temperature is correspondingly the temperature that a flow medium has at the inlet into a turbo machine.

25 In today's turbo machines, cooling steam with the characteristic variables described above of temperature and pressure is not produced by the machine itself.

The cooling steam required is generally supplied to the 30 turbo machine through a separate line. In the case of turbo machines with multi-stage superheater stages, the cooling steam is usually removed from an associated boiler upstream of the last superheater stage and passed to the turbo machine in a separate line. The 35 disadvantage of this solution is that a separate line causes additional costs. In addition, a direct dependence on the boiler arises to the extent that the dimensioning of the cooling steam system depends on the

boiler parameters and that failure of the cooling steam supply likewise leads to failure of the cooling.

The object of the invention is to provide a method with
5 which the provision of cooling steam is less susceptible to problems. Furthermore, a turbo machine for which the aforementioned method is used is to be provided.

10 The object directed at the method is achieved in that, for cooling thermally highly stressed regions in a turbo machine which has a live-steam feed line, an inflow region, a housing and an exhaust-steam region, a flow medium flowing through the turbo machine and
15 leaving in the exhaust-steam region during operation, part of the flow medium from the live-steam feed line is cooled in a heat exchanger before entry into the turbo machine and enters the turbo machine via the inflow region, thermally highly stressed components
20 that are located in the inflow region being cooled by the flow medium that has been cooled in this way. By this method it is possible to provide cooling steam without using a separate external line for the supply
25 of cooling steam. The cooling steam is virtually generated by the turbo machine itself.

In an advantageous development, the heat exchanger is located in the exhaust-steam region of the turbo machine. This measure achieves the effect that an
30 external cooling source does not have to be used as the cooling source. This has the effect of creating as it were an autonomous system.

In an advantageous development of the method, a shut-off valve is arranged in the live-steam feed line and the part of the flow medium that passes directly to the exhaust-steam region is branched off downstream of the shut-off valve. This creates the possibility of

quickly interrupting the steam supply to the turbo machine by actuating the quick-closure valve in the event of a problem occurring.

5 In an advantageous development of the method, the method is used for turbo machines which have a heat exchanger which is distinguished by the fact that the part of the flow medium that flows through the heat exchanger is cooled by at least 10°C below the
10 temperature of the live steam. In particular, the heat exchanger may be distinguished by the fact that the part of the flow medium that flows through the heat exchanger is cooled by at least 20°C below the temperature of the live steam.

15 In an advantageous development of the method, the method is used for a turbo machine which has a thrust-compensating piston, the cooling steam generated in the method being passed to the thermally stressed thrust-
20 compensating piston. This creates the possibility of cooling a thermally stressed component, such as the thrust-compensating piston, autonomously without a separate cooling steam line.

25 The object directed at the device is achieved by a turbo machine which has a live-steam feed line through which a flow medium can flow and which leads to a live-steam inflow region, the turbo machine having an outflow region, the live-steam feed line having a
30 branch with which part of the flow medium is passed via a line to a heat exchanger, and the turbo machine having a feed line downstream of the heat exchanger into an inflow region. By this novel arrangement of the cooling-steam feed line it is possible to provide
35 cooling steam without laying a separate external line. The cooling steam is virtually generated by the turbo machine itself.

In an advantageous development, the heat exchanger is arranged in the exhaust-steam region of the turbo machine. This measure achieves the effect that an external cooling source does not have to be used as the 5 cooling source. This has the effect of creating as it were an autonomous system.

In an advantageous development of the device, a shut-off valve is located in the live-steam feed line, the 10 branching of the live-steam feed line to the heat exchanger taking place just downstream of the shut-off valve. This achieves the effect that the live-steam feed line, and consequently also the cooling feed line, can be interrupted in the event of a problem arising.

15 In a further advantageous development of the device, the generated cooling steam is passed directly to the thrust-compensating piston of the steam turbine. This has the effect of specifically cooling a region which 20 is thermally stressed in a turbo machine.

An exemplary embodiment of the invention is explained in more detail on the basis of a drawing.

25 In the figures of the drawings specifically:

Figure 1 shows the cross section of a turbo machine;

30 Figure 2 shows a basic diagram of the cooling steam generation.

The same reference numerals are used throughout the following text for parts that are the same or have the same function.

35 In Figure 1, a turbo machine 1 is represented. The turbo machine 1 has a housing 2. An inner housing 3 is arranged in such a way that a shaft 4 is rotatable

within the inner housing 3. The inner housing 3 has guiding blades 5. The shaft 4 has moving blades 6. A heat exchanger 8 is arranged in the exhaust-steam region 7. The heat exchanger does not have to be
5 arranged in the exhaust-steam region 7 of the turbo machine 1.

The live steam is passed to the turbo machine 1 from a boiler (not represented) via the live-steam feed line
10 9. At the branch 10, part of the live steam is passed to the heat exchanger 8. The temperature of the live steam upstream of this branch 10 may be around 565°C and the pressure around 250 bar. The remaining part of the live steam, i.e. the part that is not passed to the
15 heat exchanger, passes via the line 11 into the turbo machine 1. The live steam thereby passes into the live-steam inflow region 12 and, from there, the flow medium flows through the guiding blades and moving blades 5, 6 along the axial direction 13. After the
20 final row of blades 14, which comprises a row of guiding blades and moving blades 5 and 6, the cooled and expanded live steam passes into the exhaust-steam region 7. The temperature may then be 330°C. The pressure may be around 55 bar.

25 The heat exchanger 8 is designed in such a way that the flow medium leaving downstream of the heat exchanger 8 is cooled by at least 10°C, in particular by at least 20°C, with respect to the flow medium entering the heat
30 exchanger upstream of it.

The live steam cooled in this way passes via the discharge line 16 into the inflow region 17 of the turbo machine 1. The inflow region 17 is separated
35 from the live-steam inflow region 12 by means of a guiding blade ring 18 in such a way that the cooled live steam that comes from the discharge line 16 passes into the inflow region 17. From there, the cooled live

steam passes to the thermally stressed thrust-compensating piston 19 or to other thermally stressed regions. The thermally stressed regions of the shaft 4 in the inflow region 17 are cooled by the cooled live steam.

In Figure 2, a basic diagram of the cooling arrangement can be seen. Live steam passes via a live-steam feed line 9 to the turbo machine 1. The live-steam feed line 9 has a shut-off valve 20. The shut-off valve 20 is fitted upstream of a branch 10. The branch 10 leads to a branching of live steam via a feed line 15 to the heat exchanger 8. The branched-off live steam is cooled in the heat exchanger 8 and passes via the discharge line 16 into the inflow region 17. The direction of flow of the cooling steam 21 is represented by the arrows 21. The cooling steam is passed around the thrust-compensating piston 19 and in this way cools this thermally stressed region. The inflow region 17 is separated from the live-steam inflow region 12 by means of a guiding blade ring 18.

The part of the live steam that passes via the live-steam feed line 9 and the line 11 to the turbo machine 1 flows over guiding blades and moving blades (not represented in Figure 2) in the direction of the arrow 22 through the turbo machine 1 and leaves the turbo machine 1 in the exhaust-steam region 7. The guiding blade ring 18 is fitted in such a way that the cooling steam can be introduced into the turbo machine 1. All that is required for this purpose is that the pressure loss in the heat exchanger 8 that is used is lower than the pressure reduction over this guiding blade ring 18, in order to obtain a driving pressure differential. The heat exchanger 8 located in the exhaust-steam flow 23 of the turbo machine 1 cools down the live steam coming via the feed line 15 and gives off the excess heat to the exhaust steam, it being possible if

appropriate for this excess heat to be saved in a downstream reheat cycle that is not represented. As a result, no additional losses occur.

- 5 The live steam required for the cooling can be removed downstream of the shut-off valve 20. This has the effect that the entire system is self-regulating, i.e. no additional shut-off or control devices are required.
- 10 independent of a boiler (not represented) and other components. In other words, the cooling steam required is generated by the turbine itself and in this way makes it independent of external components. This variant is simple and inexpensive, since the generation
- 15 of the cooling steam takes place with a heat exchanger 8 installed in the feed line 15.